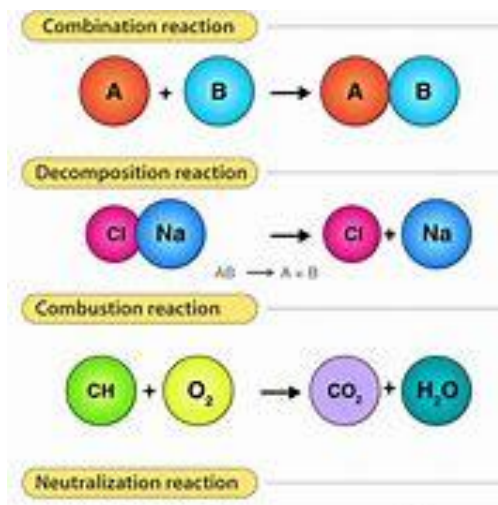
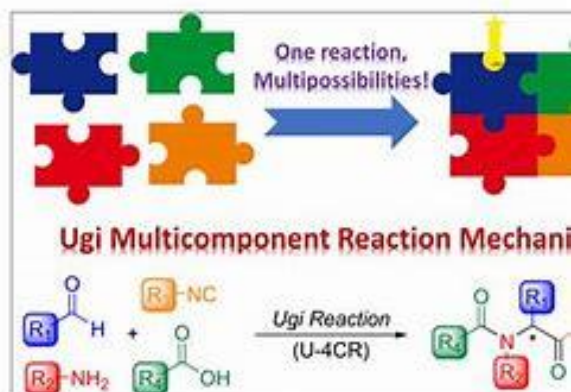


Reactor Design II



Week 3 Multiple Reactions

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Introduction

- Chemical Reaction Engineering (CRE) examines the dynamics of reaction rates, mechanisms, and reactor design.
- This lecture focuses on multiple reactions, their classification, and strategies to optimize selectivity and yield.

Topics to be Addressed

- - Fundamentals of Multiple Reactions
- - Types of Reactions: Series, Parallel, Independent, and Complex
- - Selectivity and Yield: Instantaneous vs. Overall
- - Analytical and Numerical Approaches
- - Case Studies and Practical Applications

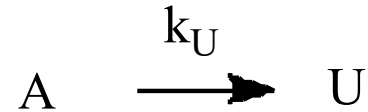
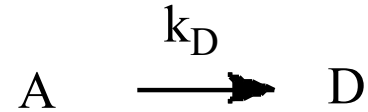
Objectives

- By the end of this lecture, students will be able to:
 - - Classify multiple reaction types and their characteristics.
 - - Apply mole balances, rate laws, and stoichiometry to multiple reactions.
 - - Analyze selectivity and yield in reaction networks.
 - - Develop strategies to maximize desired products in complex reactions.

Introduction

- Multiple reactions, including series, parallel, independent, and complex types, play a critical role in chemical process optimization.
- This session explores theoretical insights and practical approaches to analyze and maximize the desired products.

- Multiple Reactions



- Selectivity and Yield

- Series Reactions



- Complex Reactions



Types of Multiple Reactions

- Series: $A \rightarrow B \rightarrow C$
- Parallel: $A \rightarrow D$
 $A \rightarrow U$
- Independent: $A \rightarrow B$
 $C \rightarrow D$
- Complex: $A + B \rightarrow C + D$
 $A + C \rightarrow E$

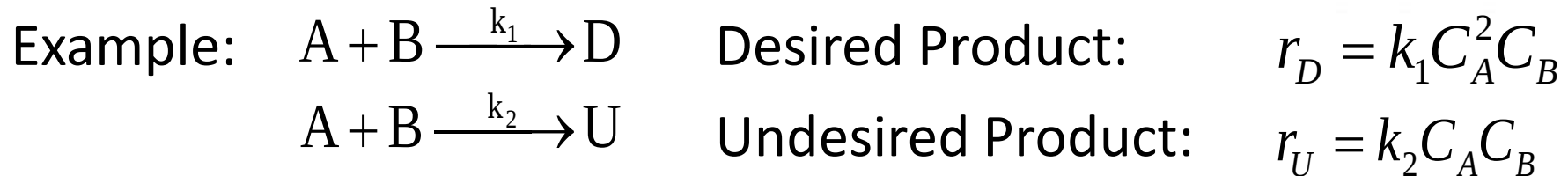
With multiple reactors, either molar flow or number of moles must be used (no conversion!)

Selectivity and Yield

There are two types of selectivity and yield:
Instantaneous and Overall.

	Instantaneous	Overall
Selectivity	$S_{DU} = \frac{r_D}{r_U}$	$\tilde{S}_{DU} = \frac{F_D}{F_U}$
Yield	$Y_D = \frac{r_D}{-r_A}$	$\tilde{Y}_D = \frac{F_D}{F_{A0} - F_A}$

Selectivity and Yield



$$S_{D/U} = \frac{r_D}{r_U} = \frac{k_1 C_A^2 C_B}{k_2 C_A C_B} = \frac{k_1}{k_2} C_A$$

To maximize the selectivity of D with respect to U run at high concentration of A and use **PFR**.

Gas Phase: Multiple Reactions



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Following the Algorithm

Number all reactions

Mole balances:

Mole balance on each and every species

PFR
$$\frac{dF_j}{dV} = r_j$$

CSTR
$$F_{j0} - F_j = -r_j V$$

Batch
$$\frac{dN_j}{dt} = r_j V$$

Membrane ("i" diffuses in)
$$\frac{dF_i}{dV} = r_i + R_i$$

Liquid-semibatch
$$\frac{dC_j}{dt} = r_j + \frac{v_0(C_{j0} - C_j)}{V}$$

Rates:

Laws
$$r_{ij} = k_{ij} f_i(C_j, C_n)$$

Relative rates
$$\frac{r_{iA}}{-a_i} = \frac{r_{iB}}{-b_i} = \frac{r_{iC}}{c_i} = \frac{r_{iD}}{d_i}$$

Net rates
$$r_j = \sum_{i=1}^q r_{ij}$$

Stoichiometry:

Gas phase

$$C_j = C_{T0} \frac{F_j P T_0}{F_T P_0 T} = C_{T0} \frac{F_j T_0}{F_T T} y$$

$$p = \frac{P}{P_0}$$

$$F_T = \sum_{j=1}^n F_j$$

$$\frac{dp}{dW} = -\frac{\alpha}{2p} \left(\frac{F_T}{F_{T0}} \right) \frac{T}{T_0}$$

Liquid phase

$$v = v_0$$

$$C_A, C_B, \dots$$

Combine:

Polymath will combine all the equations for you. Thank you.

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Multiple Reactions

A) **Mole Balance** of each and every species

Flow

$$\frac{dF_A}{dV} = r_A$$

$$\frac{dF_B}{dV} = r_B$$

Batch

$$\frac{dN_A}{dt} = r_A V$$

$$\frac{dN_B}{dt} = r_B V$$

Multiple Reactions

B) Rates

$$-r_{1A} = k_{1A} C_A C_B$$

a) **Rate Law** for each reaction:

$$-r_{2A} = k_{2A} C_C C_A$$

$$r_A = \sum_{i=1} r_{iA} = r_{1A} + r_{2A}$$

b) Net **Rates**:

$$\frac{r_{iA}}{-a_i} = \frac{r_{iB}}{-b_i} = \frac{r_{iC}}{c_i} = \frac{r_{iD}}{d_i}$$

c) Relative **Rates**:

Multiple Reactions

C) Stoichiometry

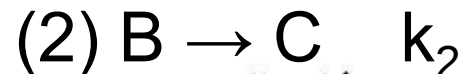
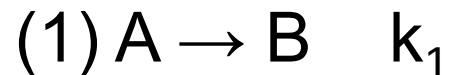
$$C_A = C_{T0} \frac{F_A}{F_{A0}} \left(\frac{P}{P_0} \right) \left(\frac{T_0}{T} \right)$$

Gas:

$$C_A = F_A / \nu_0$$

Liquid:

Example: $A \rightarrow B \rightarrow C$





1) Mole Balances

$$\frac{dN_A}{dt} = r_A V$$

$$\frac{dN_B}{dt} = r_B V$$

$$\frac{dN_C}{dt} = r_C V$$

$$V = V_0 \text{ (constant batch)}$$

$$\frac{dC_A}{dt} = r_A \quad \frac{dC_B}{dt} = r_B \quad \frac{dC_C}{dt} = r_C$$

2) Rate Laws

$$-r_{1A} = k_{1A} C_A$$

$$-r_{1B} = k_{1B} C_B$$

Laws

$$r_A = r_{1A}$$

$$r_B = r_{1B} + r_{2B}$$

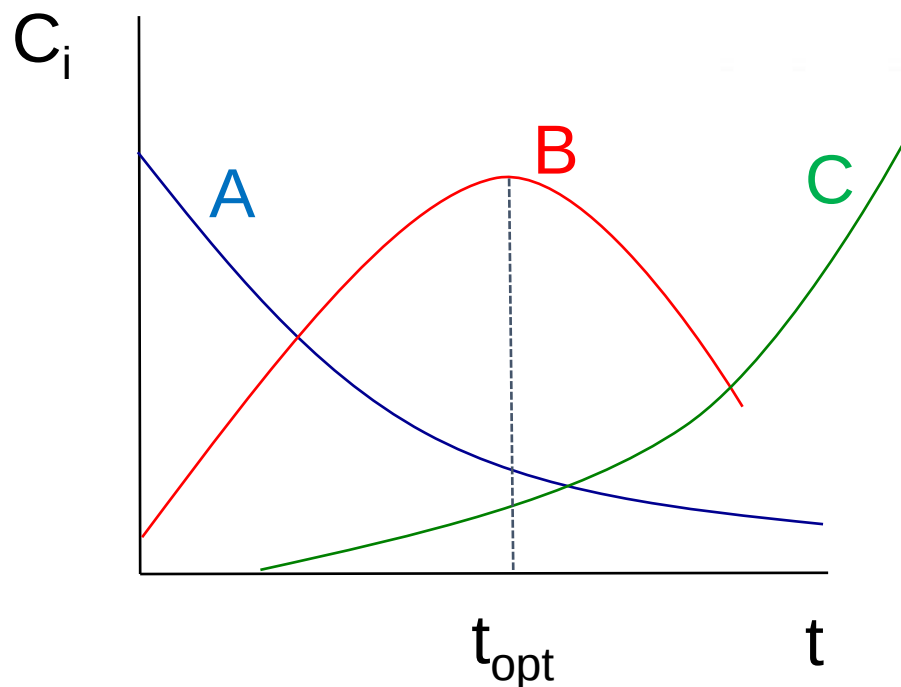
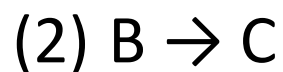
Net rates

$$\frac{r_{1A}}{-1} = \frac{r_{1B}}{1}$$

$$\frac{r_{2B}}{-1} = \frac{r_{2C}}{1}$$

Relative rates

Example 1: Batch Series Reactions



1) Mole Balances

$$\frac{dC_A}{dt} = r_A$$

$$\frac{dC_B}{dt} = r_B$$

$$V = V_o \quad \frac{dC_C}{dt} = r_C$$



2) Rate Laws

Laws: $r_{1A} = -k_1 C_A$

$$r_{2B} = -k_2 C_B$$

Relative: $\frac{r_{1A}}{-1} = \frac{r_{1B}}{1} \qquad \frac{r_{2B}}{-1} = \frac{r_{2C}}{1}$

3) Combine

Species A:
$$-\frac{dC_A}{dt} = -r_A = k_1 C_A$$

$$C_A = C_{A0} \exp(-k_1 t)$$

Species B:
$$\frac{dC_B}{dt} = r_B$$

$$r_B = r_{B\text{ NET}} = r_{1B} + r_{2B} = k_1 C_A - k_2 C_B$$

$$\frac{dC_B}{dt} + k_2 C_B = k_1 C_{A0} \exp(-k_1 t)$$

Example 1: Batch Series Reactions



Using the integrating factor, $I.F. = \exp\left(\int k_2 dt\right) = \exp(k_2 t)$

$$d \frac{[C_B \exp(k_2 t)]}{dt} = k_1 C_{A0} \exp(k_2 - k_1)t$$

at $t = 0$, $C_B = 0$

$$C_B = \frac{k_1 C_{A0}}{k_2 - k_1} \left[\exp(-k_1 t) - \exp(-k_2 t) \right]$$

$$C_C = C_{A0} - C_A - C_B$$

$$C_C = \frac{C_{A0}}{k_2 - k_1} \left[k_2 (1 - e^{-k_1 t}) - k_1 (1 - e^{-k_2 t}) \right]$$



What is the optimal τ ?

1) Mole Balances

$$\text{A:} \quad F_{A0} - F_A + r_A V = 0$$

$$C_{A0} v_0 - C_A v_0 + r_A V = 0$$

$$C_{A0} - C_A + r_A \tau = 0$$

$$\text{B:} \quad 0 - v_0 C_B + r_B V = 0$$

$$-C_B + r_B \tau = 0$$



2) Rate Laws

Laws: $r_{1A} = -k_1 C_A$

$$r_{2B} = -k_2 C_B$$

Relative: $\frac{r_{1A}}{-1} = \frac{r_{1B}}{1} \qquad \frac{r_{2B}}{-1} = \frac{r_{2C}}{1}$

Net: $r_A = r_{1A} + 0 = -k_1 C_A$

$$r_B = -r_{1A} + r_{2B} = k_1 C_A - k_2 C_B$$

Example 2: CSTR Series Reactions



3) Combine

$$C_{A0} - C_A - k_1 C_A t = 0$$

$$C_A = \frac{C_{A0}}{1 + k_1 t}$$

$$-C_B + (k_1 C_A - k_2 C_B) t = 0$$

$$C_B = \frac{k_1 C_A t}{1 + k_2 t}$$

$$C_B = \frac{k_1 C_{A0} t}{(1 + k_2 t)(1 + k_1 t)}$$

Example 2: CSTR Series Reactions



Find τ that gives maximum concentration of B

$$C_B = \frac{k_1 C_{A0} \tau}{(1 + k_2 \tau)(1 + k_1 \tau)}$$

$$\frac{dC_B}{d\tau} = 0$$

$$\tau_{\max} = \frac{1}{\sqrt{k_1 k_2}}$$



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Following the Algorithm

Number all reactions

Mole balances:

Mole balance on each and every species

$$\text{PFR} \quad \frac{dF_j}{dV} = r_j$$

$$\text{CSTR} \quad F_{j0} - F_j = -r_j V$$

$$\text{Batch} \quad \frac{dN_j}{dt} = r_j V$$

$$\text{Membrane ("i" diffuses in)} \quad \frac{dF_i}{dV} = r_i + R_i$$

$$\text{Liquid-semibatch} \quad \frac{dC_j}{dt} = r_j + \frac{v_0(C_{j0} - C_j)}{V}$$

Rates:

$$\text{Laws} \quad r_{ij} = k_{ij} f_i(C_j, C_n)$$

$$\text{Relative rates} \quad \frac{r_{iA}}{-a_i} = \frac{r_{iB}}{-b_i} = \frac{r_{iC}}{c_i} = \frac{r_{iD}}{d_i}$$

$$\text{Net rates} \quad r_j = \sum_{i=1}^q r_{ij}$$

Stoichiometry:

$$\text{Gas phase} \quad C_j = C_{T0} \frac{F_j}{F_T} \frac{P}{P_0} \frac{T_0}{T} = C_{T0} \frac{F_j}{F_T} \frac{T_0}{T} y$$

$$p = \frac{P}{P_0}$$

$$F_T = \sum_{j=1}^n F_j$$

$$\frac{dp}{dW} = - \frac{\alpha}{2p} \left(\frac{F_T}{F_{T0}} \right) \frac{T}{T_0}$$

Liquid phase

$$v = v_0$$

$$C_A, C_B, \dots$$

Combine:

Polymath will combine all the equations for you. Thank you.

Are you ready?



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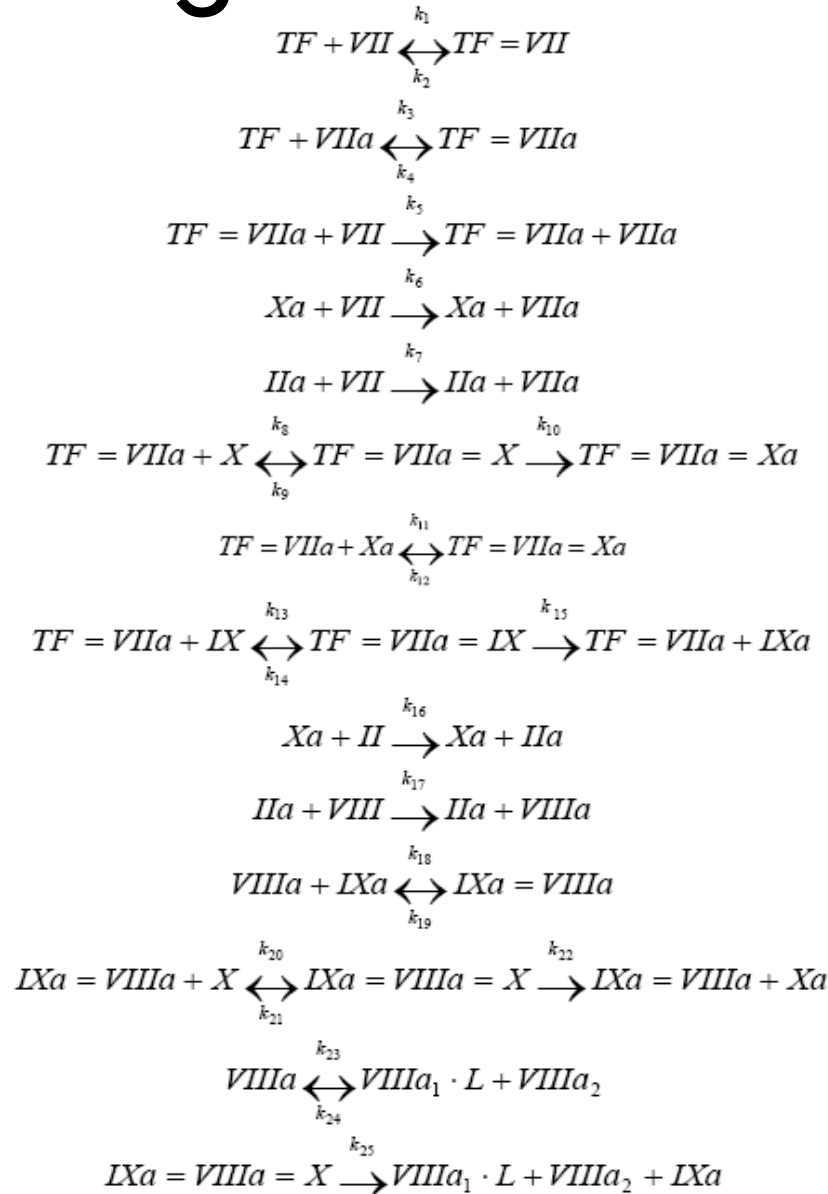
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Supplementary Slides

Blood Coagulation



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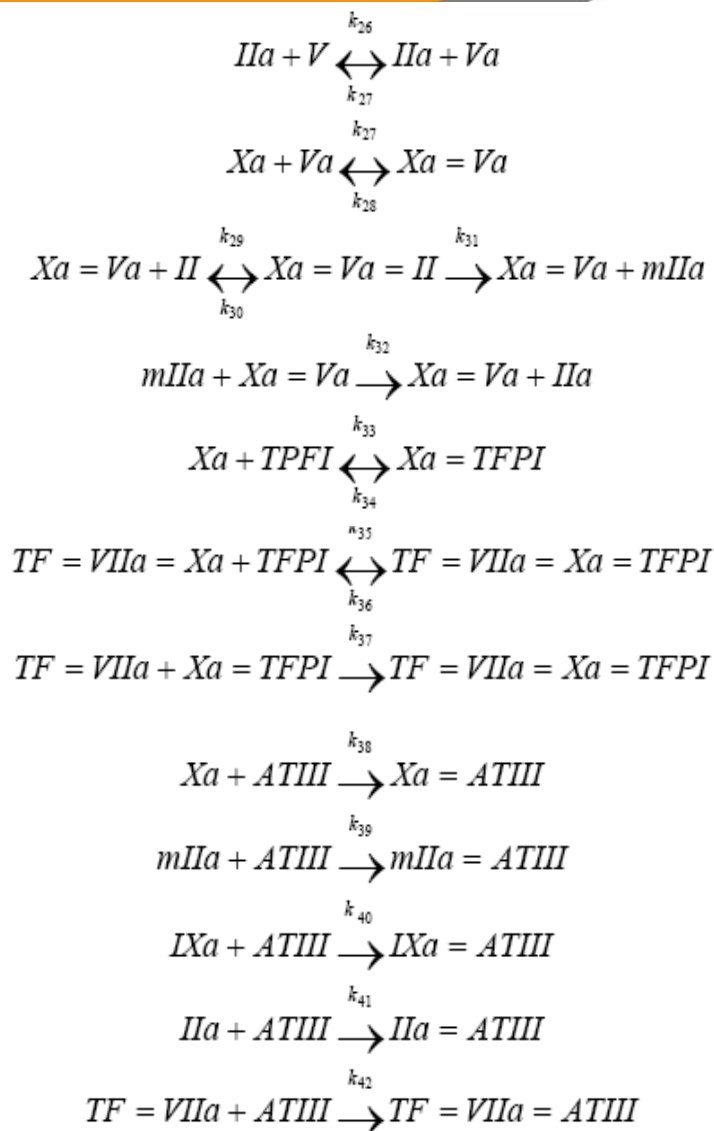


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Notations

Species symbol	Nomenclature
TF	Tissue factor
VII	proconvertin
TF=VIIa	factor TF=VIIa
VIIa	factor novoseven
TF=VIIa	factor TF=VIIa complex
Xa	Stuart prower factor activated
IIa	thrombin
X	Stuart Prower factor
TF=VIIa=X	TF=VIIa=X complex
TF=VIIa=X	TF=VIIa=X complex
IX	Plasma Thromboplastin Component
TF=VIIa=IX	TF=VIIa=IX complex
IXa	factor IXa
II	prothrombin
VIII	antihemophilic factor
VIIIa	antihemophilic factor activated
IXa=VIIIa	IXa=VIIIa complex
IXa=VIIIa=X	IXa=VIIIa=X complex

Notations

VIIIa ₁ L	factor VIIIa ₁ L
VIIIa ₂	factor VIIIa ₂
V	proaccelerin
Va	factor Va
Xa=Va	Xa=Va complex
Xa=Va=II	Xa=Va=II complex
mIIa	meizothrombin
TFPI	tissue factor pathway inhibitor
Xa=TFPI	Xa=TFPI complex
TF=VIIa=Xa=TFPI	TF=VIIa=Xa=TFPI complex
ATIII	antithrombin
Xa=ATIII	Xa=ATIII complex
mIIa=ATIII	mIIa=ATIII complex
IXa=ATIII	IXa=ATIII complex
TF=VIIIa=ATIII	TF=VIIIa=ATIII complex
IIa=ATIII	IIa=ATIII complex

Mole Balances

$$\frac{dC_{TF}}{dT} = k_2 \cdot C_{TFVII} - k_1 \cdot C_{TF} \cdot C_{VII} - k_3 \cdot C_{TF} \cdot C_{VIIa} + k_4 \cdot C_{TFVIIa}$$

$$\frac{dC_{VII}}{dt} = k_2 \cdot C_{TFVII} - k_1 \cdot C_{TF} \cdot C_{VII} - k_6 \cdot C_{Xa} \cdot C_{VII} - k_7 \cdot C_{IIa} \cdot C_{VII} - k_5 \cdot C_{TFVIIa} \cdot C_{VII}$$

$$\frac{dC_{TFVII}}{dt} = -k_2 \cdot C_{TFVII} + k_1 \cdot C_{TF} \cdot C_{VII}$$

$$\frac{dC_{VIIa}}{dt} = k_4 \cdot C_{TFVIIa} - k_3 \cdot C_{TF} \cdot C_{VIIa} + k_5 \cdot C_{TFVIIa} \cdot C_{VII} + k_6 \cdot C_{Xa} \cdot C_{VII} + k_7 \cdot C_{IIa} \cdot C_{VII}$$

$$\frac{dC_{TFVIIa}}{dt} = -k_4 \cdot C_{TFVIIa} + k_3 \cdot C_{TF} \cdot C_{VIIa} + k_9 \cdot C_{TFVIIaX} - k_8 \cdot C_{TFVIIa} \cdot C_X - k_{11} \cdot C_{TFVIIa} \cdot C_{Xa} +$$

$$k_{12} \cdot C_{TFVIIaXa} - k_{13} \cdot C_{TFVIIa} \cdot C_{IX} + k_{14} \cdot C_{TFVIIaIX} + k_{15} \cdot C_{TFVIIaIX} - k_{37} \cdot C_{TFVIIa} \cdot C_{XaTFPI} -$$

$$k_{42} \cdot C_{TFVIIa} \cdot C_{ATIII}$$

$$\frac{dC_{Xa}}{dt} = k_{11} \cdot C_{TFVIIa} \cdot C_{Xa} + k_{12} \cdot C_{TFVIIaXa} + k_{22} \cdot C_{IXaVIIIaX} + k_{28} \cdot C_{XaVa} - k_{27} \cdot C_{Xa} \cdot C_{Va} +$$

$$k_{34} \cdot C_{XaTFPI} - k_{33} \cdot C_{Xa} \cdot C_{TFPI} - k_{38} \cdot C_{Xa} \cdot C_{ATIII}$$

$$\frac{dC_{IIa}}{dt} = k_{16} \cdot C_{Xa} \cdot C_{II} + k_{32} \cdot C_{mIIa} \cdot C_{XaVa} - k_{41} \cdot C_{IIa} \cdot C_{ATIII}$$

$$\frac{dC_X}{dt} = -k_8 \cdot C_{TFVIIa} \cdot C_X + k_9 \cdot C_{TFVIIaX} - k_{20} \cdot C_{IXaVIIIa} \cdot C_X + k_{21} \cdot C_{IXaVIIIaX} + k_{25} \cdot C_{IXaVIIIaX}$$

$$\frac{dC_{TFVIIaX}}{dt} = k_8 \cdot C_{TFVIIa} \cdot C_X - k_9 \cdot C_{TFVIIaX} - k_{10} \cdot C_{TFVIIaX}$$



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Mole Balances

$$\frac{dC_{TFVTHaXa}}{dt} = k_{10} \cdot C_{TFVTHaX} + k_{11} \cdot C_{TFVTHa} \cdot C_{Xa} - k_{12} \cdot C_{TFVTHaXa} + k_{36} \cdot C_{TFVTHaXaTFPI} - k_{35} \cdot C_{TFVTHaNa} \cdot C_{TFPI}$$

$$\frac{dC_{IX}}{dt} = k_{14} \cdot C_{TFVTHaIX} - k_{13} \cdot C_{TFVTHa} \cdot C_{IX}$$

$$\frac{dC_{TFVTHaIX}}{dt} = -k_{14} \cdot C_{TFVTHaIX} + k_{13} \cdot C_{TFVTHa} \cdot C_{IX} - k_{15} \cdot C_{TFVTHaIX}$$

$$\frac{dC_{IXa}}{dt} = k_{15} \cdot C_{TFVTHaIX} - k_{18} \cdot C_{VIIIa} \cdot C_{IXa} + k_{19} \cdot C_{IXaVIIIa} + k_{25} \cdot C_{IXaVIIIaX} - k_{40} \cdot C_{IXa} \cdot C_{ATIII}$$

$$\frac{dC_{II}}{dt} = -k_{16} \cdot C_{Xa} \cdot C_{II} + k_{30} \cdot C_{XaVaII} - k_{29} \cdot C_{XaVa} \cdot C_{II}$$

$$\frac{dC_{VIII}}{dt} = -k_{17} \cdot C_{IIa} \cdot C_{VIII}$$

$$\frac{dC_{VIIIa}}{dt} = k_{17} \cdot C_{IIa} \cdot C_{VIII} - k_{18} \cdot C_{VIIIa} \cdot C_{IXa} + k_{19} \cdot C_{IXaVIIIa} - k_{23} \cdot C_{VIIIa} + k_{24} \cdot C_{VIIIa_1L}$$

$$\frac{dC_{IXaVIIIa}}{dt} = k_{18} \cdot C_{VIIIa} \cdot C_{IXa} - k_{19} \cdot C_{IXaVIIIa} + k_{21} \cdot C_{IXaVIIIaX} - k_{20} \cdot C_{IXaVIIIa} \cdot C_X + k_{22} \cdot C_{IXaVIIIaX}$$

$$\frac{dC_{IXaVIIIaX}}{dt} = -k_{21} \cdot C_{IXaVIIIaX} + k_{20} \cdot C_{IXaVIIIa} \cdot C_X - k_{22} \cdot C_{IXaVIIIaX} - k_{25} \cdot C_{IXaVIIIaX}$$

$$\frac{dC_{VIIIa_1L}}{dt} = k_{23} \cdot C_{VIIIa} - k_{24} \cdot C_{VIIIa_1L} \cdot C_{VIIIa_1} + k_{25} \cdot C_{IXaVIIIaX}$$

$$\text{COLLEGE (} \frac{dC_{VIIIa_2}}{dt} = k_{23} \cdot C_{VIIIa} - k_{24} \cdot C_{VIIIa_1L} \cdot C_{VIIIa_2} + k_{25} \cdot C_{IXaVIIIaX}$$



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Mole Balances

$$\frac{dC_V}{dt} = -k_{26} \cdot C_{IIa} \cdot C_V$$

$$\frac{dC_{Va}}{dt} = k_{26} \cdot C_{IIa} \cdot C_V + k_{28} \cdot C_{Xa} \cdot C_{Va} - k_{27} \cdot C_{Xa} \cdot C_{Va}$$

$$\frac{dC_{XaVa}}{dt} = -k_{28} \cdot C_{Xa} \cdot C_{Va} + k_{27} \cdot C_{Xa} \cdot C_{Va} - k_{29} \cdot C_{IIaVa} \cdot C_{II} + k_{30} \cdot C_{XaValI} + k_{31} \cdot C_{XaValII}$$

$$\frac{dC_{XaValI}}{dt} = k_{29} \cdot C_{IIaVa} \cdot C_{II} - k_{30} \cdot C_{XaValI} - k_{31} \cdot C_{XaValII}$$

$$\frac{dC_{mIIa}}{dt} = k_{31} \cdot C_{XaValII} - k_{32} \cdot C_{mIIa} \cdot C_{XaVa} - k_{39} \cdot C_{mIIa} \cdot C_{ATHI}$$

$$\frac{dC_{TFPI}}{dt} = k_{34} \cdot C_{XaTFPI} - k_{33} \cdot C_{Xa} \cdot C_{TFPI} + k_{36} \cdot C_{TFVIIaXaTFPI} - k_{35} \cdot C_{TFVIIaXa} \cdot C_{TFPI}$$

$$\frac{dC_{XaTFPI}}{dt} = -k_{34} \cdot C_{XaTFPI} + k_{37} \cdot C_{Xa} \cdot C_{TFPI} - k_{37} \cdot C_{TFVIIa} \cdot C_{XaTFPI}$$

$$\frac{dC_{TFVIIaXaTFPI}}{dt} = -k_{36} \cdot C_{TFVIIaXaTFPI} + k_{35} \cdot C_{TFVIIaXa} \cdot C_{TFPI} + k_{37} \cdot C_{TFVIIa} \cdot C_{XaTFPI}$$

$$\frac{dC_{ATHI}}{dt} = -k_{38} \cdot C_{Xa} \cdot C_{ATHI} - k_{39} \cdot C_{mIIa} \cdot C_{ATHI} - k_{40} \cdot C_{IXa} \cdot C_{ATHI} - k_{41} \cdot C_{IIa} \cdot C_{ATHI} - k_{42} \cdot C_{TFVIIa} \cdot C_{ATHI}$$

$$\frac{dC_{XaATHI}}{dt} = k_{38} \cdot C_{Xa} \cdot C_{ATHI}$$

$$\frac{dC_{mIIaATHI}}{dt} = k_{39} \cdot C_{mIIa} \cdot C_{ATHI}$$

$$\frac{dC_{IXaATHI}}{dt} = k_{40} \cdot C_{IXa} \cdot C_{ATHI}$$

$$\frac{dC_{TFVIIaATHI}}{dt} = k_{42} \cdot C_{TFVIIa} \cdot C_{ATHI}$$

$$\frac{dC_{IIaATHI}}{dt} = k_{41} \cdot C_{IIa} \cdot C_{ATHI}$$

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Results

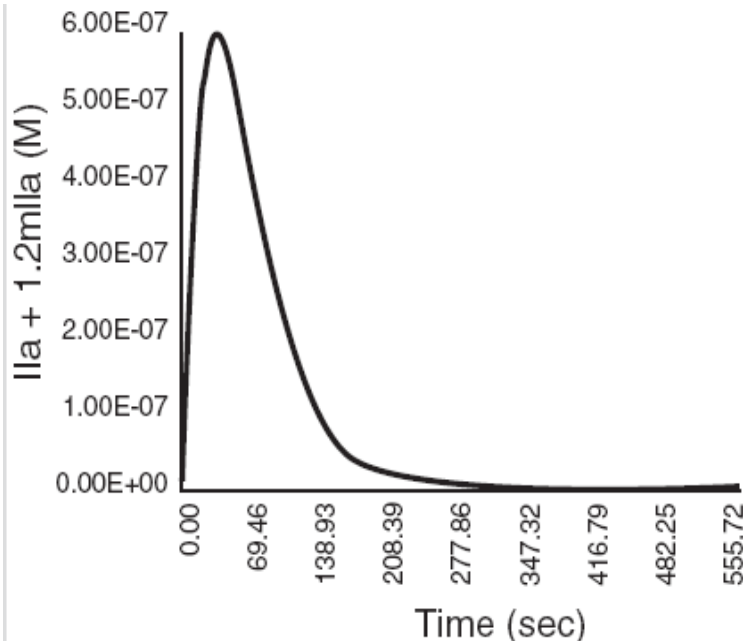


Figure D. Total thrombin as a function of time with an initiating TF concentration of 25 pM (after running Polymath) for the abbreviated blood clotting cascade.

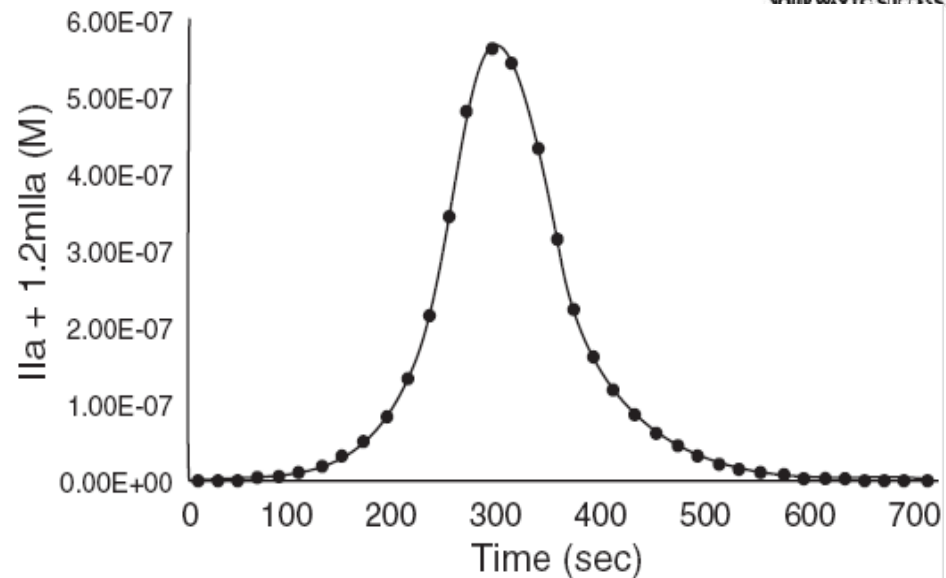


Figure E. Total thrombin as a function of time with an initiating TF concentration of 25 pM. [Figure courtesy of M. F. Hockin et al., “A Model for the Stoichiometric Regulation of Blood Coagulation,” *The Journal of Biological Chemistry*, 277[21], pp. 18322–18333 (2002)]. Full blood clotting cascade.

Blood Coagulation

Many metabolic reactions involve a large number of sequential reactions, such as those that occur in the coagulation of blood.

Cut → Blood → Clotting



Figure A. Normal Clot Coagulation of blood

(picture courtesy of: Mebs, Venomous and Poisonous Animals, Medpharm, Stugart 2002, Page 305)

Schematic of Blood Coagulation

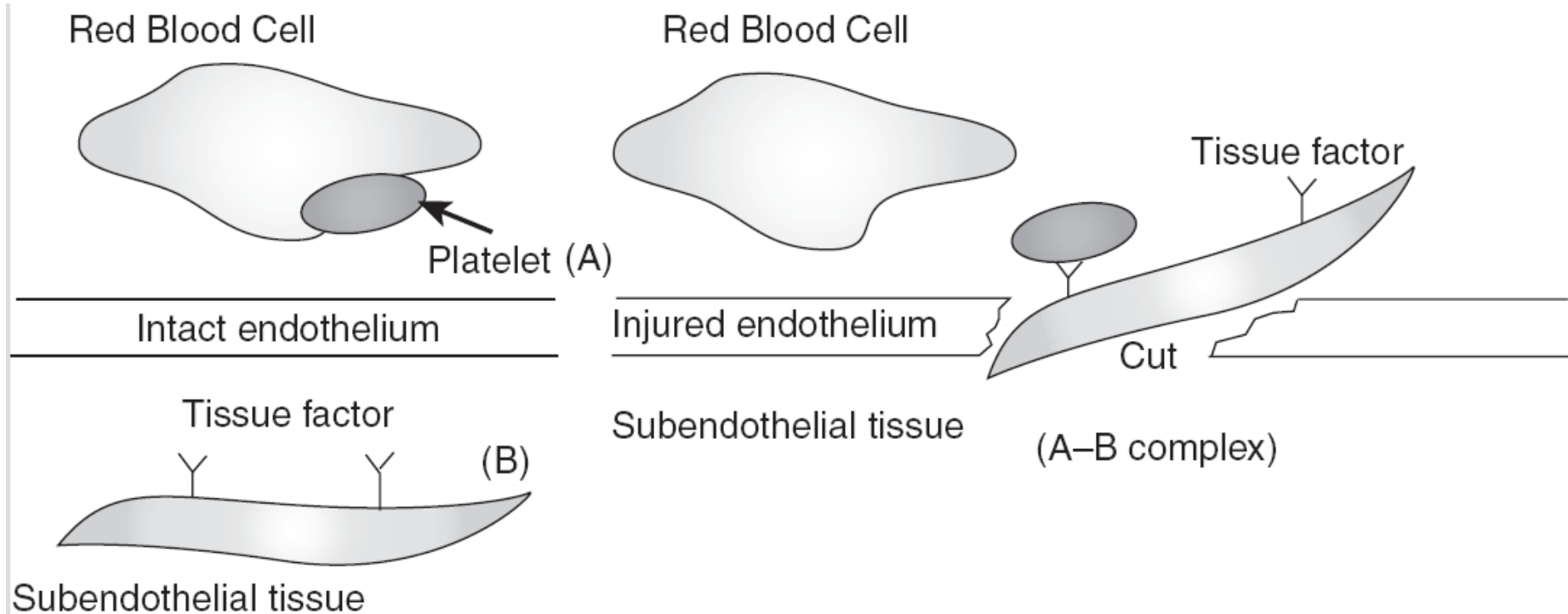


Figure B. Schematic of separation of TF (A) and plasma (B) before cut occurs.

Figure C. Cut allows contact of plasma to initiate coagulation. $(A + B \rightarrow \text{Cascade})$



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Cut



A + B



C



D



E



F



Clot

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جامعة تكريت - Tikrit University

Summary

- In this lecture, we covered:
 - - Classification and characteristics of multiple reactions.
 - - Key concepts: selectivity, yield, mole balances, and stoichiometry.
 - - Practical strategies to maximize selectivity and desired outcomes.
 - - Analytical and numerical methods for reactor performance evaluation.
- Multiple reactions are essential for understanding and optimizing complex chemical processes.